





**Bruchzähigkeitsmessung grobkörniger Ni-Basis-Legierungen  
im Hochtemperaturbereich bis 1000°C**

**Klaus F. Stärk, Carlo M. Maggi**

**47. Tagung DVM-Arbeitskreis Bruchvorgänge  
Februar 2015 Freiberg**

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**Bruchzähigkeit grobkörniger  
Ni-Basislegierungen**

**Gliederung**

- **Ni-Basis-Guss (MarM247cc)**
- **HT-Bruchzähigkeitsmessung**
- **DUPLEX-Potentialsonde**
- **Bruchflächen und Auswertung**
- **Gültigkeitskriterien**
- **Streuung und Statistik**
- **Zusammenfassung**

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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### Gliederung

- Ni-Basis-Guss (MarM247cc)

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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### Ni-Basis-Guss MarM247cc

#### Schaufelfuss



#### Schaufelblatt

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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### Ni-Basis-Guss MarM247cc



typische Gusserstarrung



Schliff durch  
1"-CT-Probe

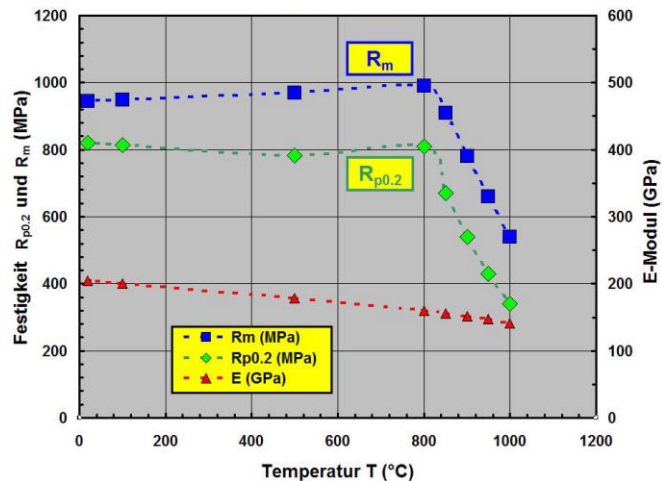
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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### Ni-Basis-Guss MarM247cc



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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### Gliederung

- Ni-Basis-Guss (MarM247cc)
- HT-Bruchzähigkeitsmessung

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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### HT-Bruchzähigkeitsmessung

Rissverlängerung/Heizung	Widerstand	Strahlung	Induktion	Gas
Teilentlastungsverfahren	✓			
Potentialsondenverfahren	✓✓		✓	

☹ schlecht  
😊 machbar  
☺ gut

- vorhandene Erfahrung
- vorhandene Ausrüstung
- vorhandene Mittel

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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### HT-Bruchzähigkeitsmessung

Rissverlängerung/Heizung	Widerstand	Strahlung	Induktion	Gas
Teilentlastungsverfahren	☹️☹️	☹️	☹️	☹️☹️
Potentialsondenverfahren	☺️	☹️☹️	☹️☹️	☺️☺️

### ➔ Potentialsonde + Gasheizung

#### Gründe:

- kontinuierliche Messung mit PD
- konstante Temperatur
- gleichmässige und hohe Temperatur
- kurze Aufheiz- und Abkühlzeiten

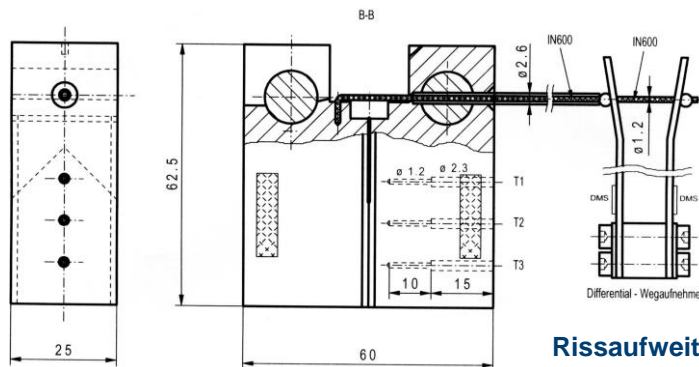
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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### HT-Bruchzähigkeitsmessung



Rissaufweitung

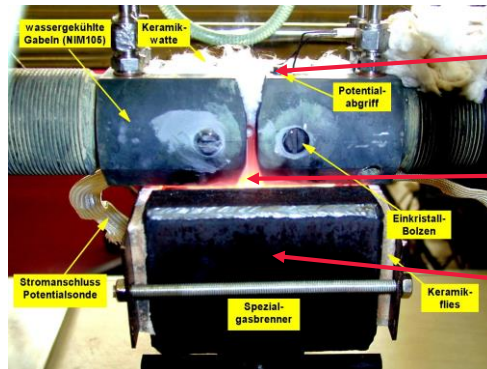
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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### HT-Bruchzähigkeitsmessung



Potential-abgriff

1''CT-Probe

Erdgas-Flächen-brenner (U-Form)

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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### Gliederung

- Ni-Basis-Guss (MarM247cc)
- HT-Bruchzähigkeitsmessung
- DUPLEX-Potentialsonde

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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### DUPLEX Potentialsonde mit Stromumkehr (DC/AC) → Widerstandsmessung

- $R = f$  (Risslänge)
- $R = f$  (Probengeometrie)
- $R = f$  (Material)
- $R = f$  (Temperatur)
- $R = f$  (Probenbeanspruchung)
- $R = f$  (Rissflächenkontakte)

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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### DUPLEX Potentialsonde mit Stromumkehr (DC/AC) → Widerstandsmessung

- $R = f$  (Risslänge) → Ziel
- $R = f$  (Probengeometrie) → Kalibrierung
- $R = f$  (Material) →  $R/R_0 = f(a/W)$
- $R = f$  (Temperatur) →  $R/R_0 = f(a/W)$
- $R = f$  (Probenbeanspruchung) → eliminieren
- $R = f$  (Rissflächenkontakte) → bewerten

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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### DUPLEX Potentialsonde Rohdaten Potentialsonde



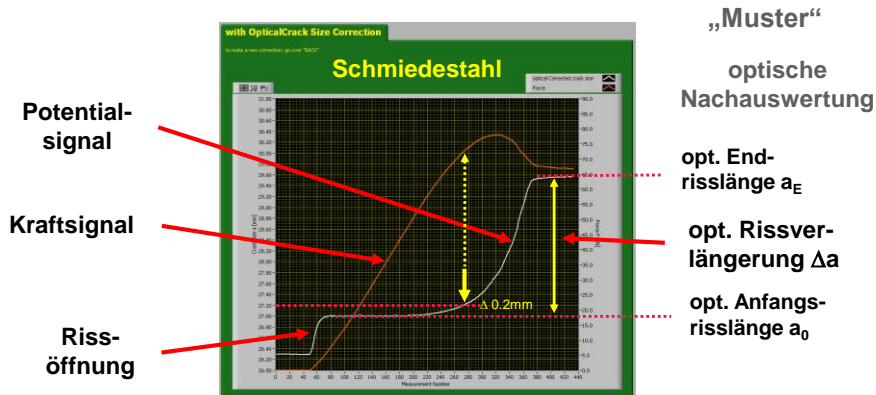
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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### DUPLEX Potentialsonde Rohdaten Potentialsonde



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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### Gliederung

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- HT-Bruchzähigkeitsmessung
- DUPLEX-Potentialsonde
- Bruchflächen und Auswertung

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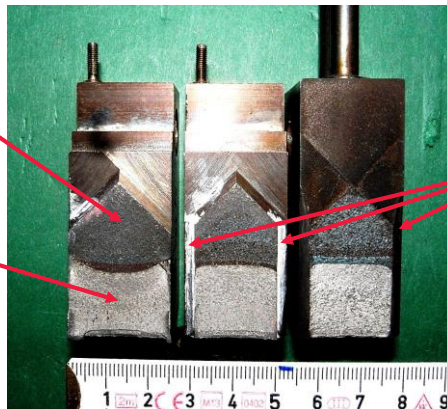


### Bruchflächen und Auswertung

Bruch-  
zähigkeit    Bruch-  
zähigkeit    Kriechriss-  
wachstum

Chevron-  
kerbe

1"- CT  
ohne  
Seiten-  
kerben



1"- CT  
mit  
Seiten-  
kerben  
2x10%

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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### Bruchflächen und Auswertung



### Nickel-Basis-Guss

### optische Bruchflächen-Nachauswertung

(RT und 550°C mit heat tinting)

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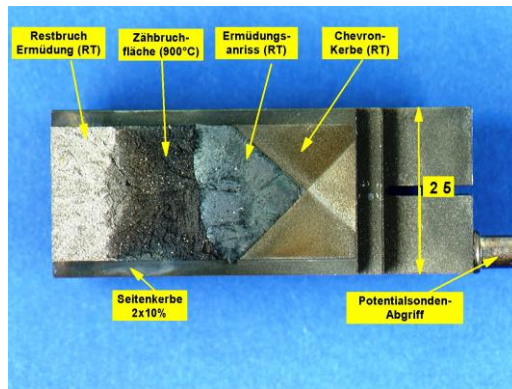
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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### Bruchflächen und Auswertung



### optische Bruchflächen-Nachauswertung

### Ni-Basis-Guss

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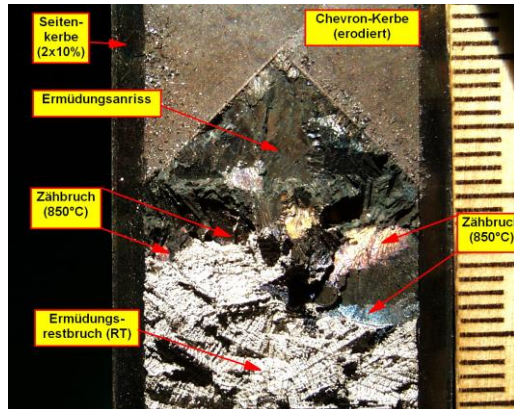
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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### Bruchflächen und Auswertung



optische  
Bruchflächen-  
Nachauswertung  
Ni-Basis-Guss

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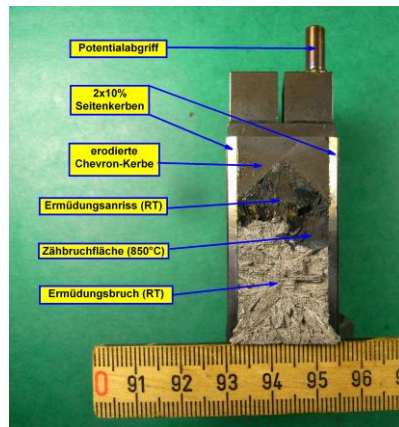
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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### Bruchflächen und Auswertung



optische  
Bruchflächen-  
Nachauswertung  
Ni-Basis-Guss

ungültige  
Rissgeometrie !!!  
 $a_r = a_m \pm 0.05B$   
 ( $\pm 1.25$  mm für 1"- CT)  
 Riss-Schräglage  $< \pm 10^\circ$

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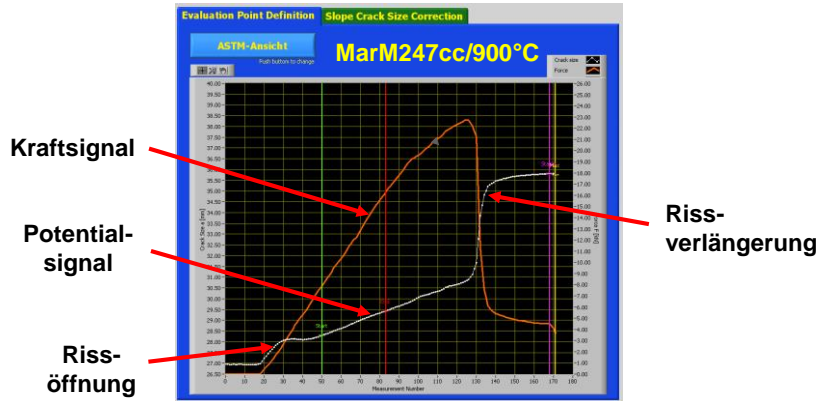


## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### Auswertung

#### Rohdaten Potentialsonde



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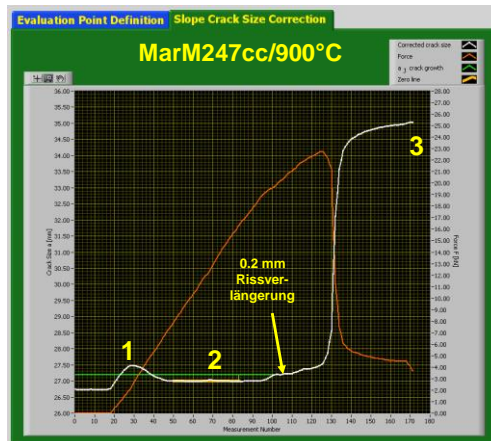
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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### Auswertung



- 1 Korrektur Ende Rissöffnung
- 2 Korrektur Materialwiderstand
- 3 Korrektur gemessene/optische Rissverlängerung (opt. Nachauswertung)

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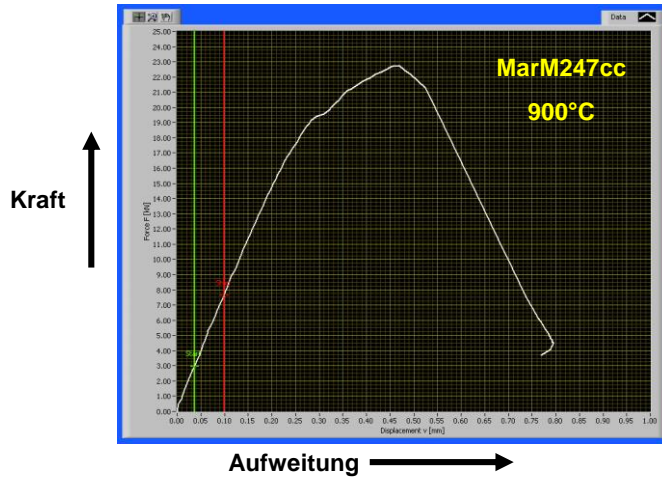
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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### Auswertung



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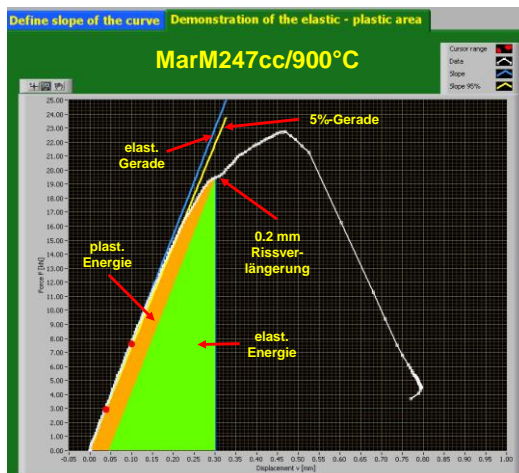
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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### Auswertung



### Berechnung

- $K_{I5\%}$
- $K_{JIC}$
- $K_{Imax}$

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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### Gliederung

- Ni-Basis-Guss (MarM247cc)
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- DUPLEX-Potentialsonde
- Bruchflächen und Auswertung
- Gültigkeitskriterien

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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### Gültigkeitskriterien

#### ASTM E399

Required for valid $K_{Ic}$		Lower Limit	Value	Upper Limit	Validity	Standard			
$F_{max} / F_Q$ Criterion:	$\frac{F_{max}}{F_Q} =$	1.439	$\leq$	1.10	Not fulfilled	E 1820 & E 399			
Ligament Criterion:	$W - a_0 =$	13.70	$<$	21.000	mm	Fulfilled	E 1820 & E 399		
Crack Size Criterion:	$\frac{a}{W} =$	0.45	$\leq$	0.580	$\leq$	0.55	mm	Not fulfilled	E 1820 & E 399
$dK/dt$ Criterion:	$\frac{dK}{dt} =$	0.55	$\leq$	0.803	$\leq$	2.75	$\frac{MPa \sqrt{m}}{s}$	Fulfilled	E 399
Pre-crack $K/E$ Criterion:	$\frac{K}{E} =$	0.0002	$\leq$	0.0003	$\sqrt{m}$	Fulfilled	E 399		
Pre-crack $K$ Criterion:	$K =$	26.4	$<$	24	$MPa \sqrt{m}$	Not fulfilled	E 1820 & E 399		

**und ungültige Rissgeometrie !!!**

$$a_i = a_m \pm 0.05B \quad (\pm 1.25 \text{ mm für } 1''\text{-CT})$$

**Riss-Schräglage  $< \pm 10^\circ$**

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# Bruchzähigkeit grobkörniger Ni-Basislegierungen



## Gültigkeitskriterien ASTM E1820

### Required for valid $K_{JIC}$

		Lower Limit	Value	Upper Limit	Validity	Standard
Ligament Criterion:	$W - a_0 =$	0.3	< 21.00	mm	fulfilled	E 1820
Thickness Criterion:	$B =$	0.3	< 25.00	mm	fulfilled	E 1820
$\Delta a$ Criterion:	$\Delta a =$	1.5	$\leq$ 11.93	mm	fulfilled	E 1820
Alstom Criterion:	$\Delta a =$	1.05	$\leq$ 11.931	mm	fulfilled	Alstom
Crack Size Criterion:	$\frac{a_0}{W} =$	0.45	$\leq$ 0.580	$\leq$ 0.70	fulfilled	E 1820
Pre-crack $K'$ Criterion:	$K =$	26.4	< 33.3	MPa $\sqrt{m}$	fulfilled	E 1820 & E 399

**aber ungünstige Rissgeometrie !!!**

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# Bruchzähigkeit grobkörniger Ni-Basislegierungen



## Gültigkeitskriterien

Results with optical crack size calibration		
$\Delta a_{max}$	12.00 mm	Crack elongation from the defined "Zero Crack Length" to the defined "Final Crack Length"
$\Delta a_{stab}$	11.95 mm	Crack elongation from the defined "Zero Crack Length" to the defined "Stable Crack Length"
$\Delta a_J$	0.19 mm	Cracklength for evaluating the J-values
$F(\Delta a)$	4.50 kN	Force at $\Delta a$ stable
$J_{pl}$	0.004 MPa m	Plastic part of the J-integral for $J_{IC}$
$J_{el}$	0.015 MPa m	Elastic part of the J-integral for $J_{IC}$
$J_{IC}$	0.019 MPa m	The plane-strain fracture toughness for slow rates of loading and substantial plastic deformation
$J_{max}$	0.040 MPa m	Fracture toughness of the material at an instability.
$F_{max}$	22.73 kN	The maximal force which the specimen sustained.
$K_{max}$	61 MPa $\sqrt{m}$	Stress intensity at the force $F_{max}$
$F_Q$	15.80 kN	Force at which $K_Q$ is determined
$K_Q$	40 MPa $\sqrt{m}$	Conditional result to determine the validity of $K_{IC}$
$K_{Jmax}$	81 MPa $\sqrt{m}$	$K_{Jmax}$ is the fracture instability toughness

$K_{IC}$	40 MPa $\sqrt{m}$	invalid
$K_{JIC}$ plain strain	55 MPa $\sqrt{m}$	valid
$K_{JIC}$ plain stress	53 MPa $\sqrt{m}$	valid

← **ungültig**

← **konservativ**

← **„gültig“**

**Notes**  
 $K_{JIC}$  : plain stress values should be used for conservative database issues.

**stark konservativ**

→

**ungültig**

→

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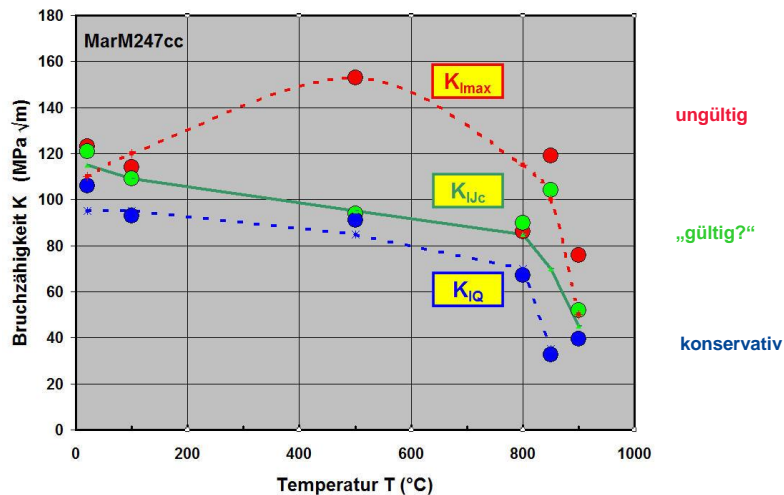
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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### Streuung und Statistik



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- Gültigkeitskriterien
- Streuung und Statistik

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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### Streuung und Statistik

#### design data

- State of the art
- Nach bestem Wissen und Gewissen
- So genau wie möglich
- Konservativ
- Statistisch notwendige Probenzahlen

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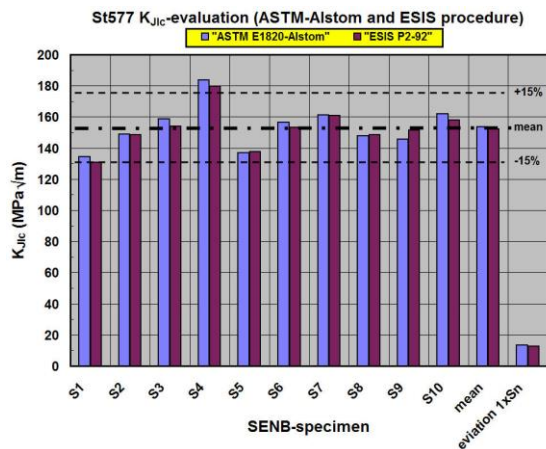
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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### Streuung und Statistik



Schmiedestahl

Chargen-  
einfluss

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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### Streuung und Statistik

#### empfohlene Probenzahl für fein- und grobkörnige Werkstoffe

- **Homogene Werkstoffe: 3 Proben pro Temperatur**
- **Homogene Werkstoffe: 3 Proben pro Charge ( $\geq 5$ )**
- **Einkristalline Werkstoffe: 3 Proben pro Orientierung ( $\geq 3$ )**
- **Grobkristalline Werkstoffe (grosse Proben):  $\geq 5$  Proben je Temperatur (mit Seitenkerben)**
- **Grobkristalline Werkstoffe (Kleinproben):  $\geq 10$  Proben je Temperatur (ohne Seitenkerben)**

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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



### Gliederung

- **Ni-Basis-Guss (MarM247cc)**
- **HT-Bruchzähigkeitsmessung**
- **DUPLEX-Potentialsonde**
- **Bruchflächen und Auswertung**
- **Gültigkeitskriterien**
- **Streuung und Statistik**
- **Zusammenfassung**

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## Bruchzähigkeit grobkörniger Ni-Basislegierungen



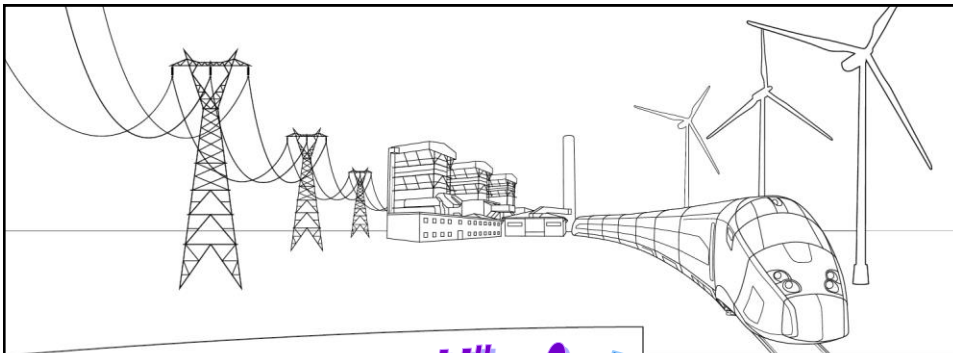
### Zusammenfassung

- Nickelbasis-Gusslegierungen (grobkörnig)
- Normen und Standards
- Schwierige Bruchzähigkeitsbestimmung
- Grosse lokale "Materialstreuung"
- Grosse Probenzahlen für Statistik erforderlich
- Proben so gross wie möglich mit Seitenkerben
  - ➔ " Werkstoffkennwert ? "
- Kleinproben mit Bauteilabmessung ohne Seitenkerben
  - ➔ " Bauteilkennwert ? "

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**Hilfe?** **Ratschläge?** **Erfahrungen?**

**Danke**  
für Ihre Aufmerksamkeit

Dr.-Ing. Klaus F. Stärk  
klaus.staerk@power.alstom.com  
klaus.staerk@swissonline.ch  
www.staerk-erdwaerme.ch

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